



PCT

WORLD INTELLECTUAL PROPERTY ORGANIZATION
International Bureau

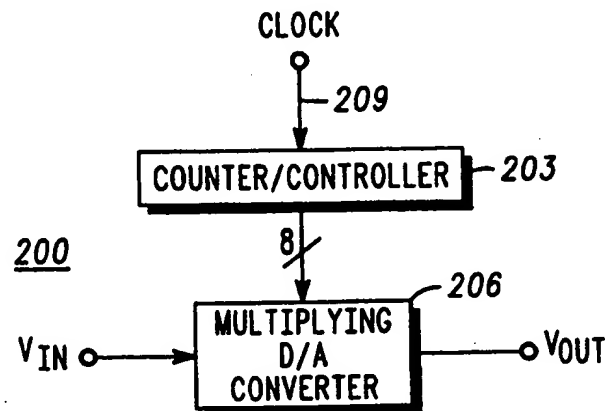
INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(15) International Patent Classification ⁵ : H03M 1/66		A1	(11) International Publication Number: WO 95/01006
			(43) International Publication Date: 5 January 1995 (05.01.95)
(21) International Application Number: PCT/US94/05419		(81) Designated States: CA, FI, GB, JP, KR, European patent (AT, BE, CH, DE, DK, ES, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE).	
(22) International Filing Date: 16 May 1994 (16.05.94)			
(30) Priority Data: 08/080,247 21 June 1993 (21.06.93) US		Published <i>With international search report.</i>	
(71) Applicant: MOTOROLA INC. [US/US]; 1303 East Algonquin Road, Schaumburg, IL 60196 (US).			
(72) Inventor: TRAYLOR, Kevin, Bruce; 7320 Holiday, North Richland Hills, TX 76180 (US).			
(74) Agents: PARMELEE, Steven, G. et al.; Motorola Inc., Intellectual Property Dept./Kab, 1303 East Algonquin Road, Schaumburg, IL 60196 (US).			

(54) Title: **APPARATUS AND METHOD FOR FREQUENCY TRANSLATION IN A COMMUNICATION DEVICE**

(57) Abstract

A digital-to-analog (D/A) convertor (206) multiplies an input signal by a sinewave approximation (300) to perform frequency translation. Optimized coefficient values are predetermined and are programmed based on a control word generated during a clock cycle. The programming over a time period representative of the frequency of the sinewave approximation (300) provides a signal that multiplies an input signal such that the effects of odd harmonics at an output are mitigated while the advantages of a traditional switching mixer are retained. In one embodiment the multiplying D/A convertor (206) includes a plurality of resistors (R1-R8) connected to an amplifier (400), with plural switching gates (G1-G8) switching select resistors (R1-R8) in and out of operation, a control word from counter/controller (203) controlling the gates (G1-G8).



FOR THE PURPOSES OF INFORMATION ONLY

Codes used to identify States party to the PCT on the front pages of pamphlets publishing international applications under the PCT.

AT	Austria	GB	United Kingdom	MR	Mauritania
AU	Australia	GE	Georgia	MW	Malawi
BB	Barbados	GN	Guinea	NE	Niger
BE	Belgium	GR	Greece	NL	Netherlands
BF	Burkina Faso	HU	Hungary	NO	Norway
BG	Bulgaria	IE	Ireland	NZ	New Zealand
BJ	Benin	IT	Italy	PL	Poland
BR	Brazil	JP	Japan	PT	Portugal
BY	Belarus	KE	Kenya	RO	Romania
CA	Canada	KG	Kyrgyzstan	RU	Russian Federation
CF	Central African Republic	KP	Democratic People's Republic of Korea	SD	Sudan
CG	Congo	KR	Republic of Korea	SE	Sweden
CH	Switzerland	KZ	Kazakhstan	SI	Slovenia
CI	Côte d'Ivoire	LI	Liechtenstein	SK	Slovakia
CM	Cameroon	LK	Sri Lanka	SN	Senegal
CN	China	LU	Luxembourg	TD	Chad
CS	Czechoslovakia	LV	Latvia	TG	Togo
CZ	Czech Republic	MC	Monaco	TJ	Tajikistan
DE	Germany	MD	Republic of Moldova	TT	Trinidad and Tobago
DK	Denmark	MG	Madagascar	UA	Ukraine
ES	Spain	ML	Mali	US	United States of America
FI	Finland	MN	Mongolia	UZ	Uzbekistan
FR	France			VN	Viet Nam
GA	Gabon				

APPARATUS AND METHOD FOR FREQUENCY TRANSLATION IN A COMMUNICATION DEVICE

5 Field of the Invention

The present invention relates generally to communication devices and more specifically to frequency translation in communication devices.

10

Background of the Invention

15 In a Direct Conversion Receiver it is often necessary to upconvert the baseband signal to an IF frequency for demodulation. One of the most popular types of mixers that is used in the frequency range of 0-5 MHz is a switching mixer which uses CMOS transmission gates to alternately change the gain applied to the baseband signal between the values of +1 and -1. The
20 gain is switched at a frequency of a local oscillator, F_{LO} .

Switching mixers have advantages such as simplicity, low offset voltage, large dynamic range, and easy to generate quadrature switching signals using D flip-flops. However, switching mixers have one major disadvantage in that the
25 baseband signal will be replicated at each odd harmonic of the clock signal, due to the fact that the multiplying signal is a square wave. Since the harmonic rolloff rate of a square wave is $1/n$, where n is the harmonic of F_{LO} , an undesired signal centered at $3F_{LO}$ will be present with a level that is approximately only 9.5 dB
30 down from the desired signal centered at F_{LO} . As the bandwidth of the baseband signal approaches F_{LO} , a bandpass filter with very steep skirt selectivity is required in order to remove the undesired harmonic signals at $3F_{LO}$ and higher.

Since the baseband signal is multiplied by the Fourier Transform of the multiplying waveform, one obvious solution to reduce the odd harmonics which appear at the output of the mixer is to use a sinewave as the multiplying signal. There are several circuit approaches which exploit the nonlinearity of transistors to accomplish this technique, however, they do not have the advantages of the switching mixer which were mentioned above. Thus a need exists for a mixer having the advantages of the switching mixer described above without the having the disadvantage of the odd harmonics at its output.

Brief Description of the Drawings

FIG. 1 generally depicts in block diagram form a prior art switching mixer.

FIG. 2 generally depicts in block diagram form a switching mixer in accordance with the invention.

FIG. 3 generally depicts a square wave and a sinewave approximation in accordance with the invention.

FIG. 4 generally depicts an embodiment of a multiplying D/A convertor in accordance with the invention.

Detailed Description of a Preferred Embodiment

The proposed invention uses a multiplying digital-to-analog (D/A) convertor and a counter to generate a stair case type multiplying signal which approximates a sinewave with frequency equal to F_{LO} . In effect, the baseband signal is multiplied by several values other than just +1 and -1 as in the simple switching mixer. The D/A convertor is clocked at a frequency that is equal to NF_{LO} and the D/A convertor has $N/2$ steps ($N/4$ positive steps and $N/4$

negative steps). FIG. 3 shows a square wave 303 and a sinewave approximation 300 generated by the proposed invention with $N=16$.

5 If the step sizes of the multiplying D/A convertor are chosen properly, sinewave approximation 300 is good enough that several of the undesired harmonic signals may be set to zero (namely those that are closest to the desired signal). In most cases the mixer in accordance with the invention will eliminate the need for a high selectivity bandpass filter and will require only a
10 simple lowpass filter to provide adequate attenuation to the harmonic signals which are not zero.

It can be shown that if the step sizes are chosen properly, the only harmonics of F_{LO} which appear at the output of the invention must satisfy the following equation.

15

$$n = iN \pm 1 \quad \text{where} \quad i = 0, 1, 2, 3, \dots$$

For the example that is shown ($N=16$), the first non zero undesired harmonic would be centered at $15F_{LO}$ compared to $3F_{LO}$ for the
20 conventional switching mixer. There will be no undesired signals centered at $3F_{LO}$, $5F_{LO}$, $7F_{LO}$, $9F_{LO}$, $11F_{LO}$ and $13F_{LO}$ at the output of the mixer in accordance with the invention. This performance would not be achievable using any finite amount of selectivity following a switching mixer. The mixer in accordance with the
25 invention gives infinite rejection to all harmonics between 2 and 14 (2 and $N-2$ for the general case) and will usually require only a simple lowpass filter to remove the 15th and higher harmonics. The mixer in accordance with the invention has all of the benefits of switching mixers mentioned above, as well as the added benefit
30 of having reduced harmonic content.

A block diagram of a prior art switching mixer 100 is shown in FIG. 1. As stated above, the switching mixer 100 alternately changes the gain applied to the baseband signal V_{in} between the

values of +1 and -1 by amplifiers 103 and 106 respectively. Gates 109 and 112 are utilized to switch between amplifiers 103 and 106 at a rate F_{10} . As stated above, this prior art switching mixer exhibits poor odd harmonic rejection at its output V_{out} .

5 FIG. 2 shows a block diagram of a switching mixer 200 in accordance with the invention. The gain applied to the baseband signal V_{in} is controlled by counter/controller 203 and a multiplying D/A convertor 206. The gain of multiplying D/A convertor 206 as a function of time is shown in FIG. 3 by the dotted
 10 sinewave approximation 300. Counter/controller 203 includes an up/down counter which automatically changes count direction when it has reached either its maximum or minimum value. For the example shown ($N=16$), the clock signal 209 has a frequency 16 times the desired frequency of sinewave approximation 300.
 15 Sinewave approximation 300 is approximated by 16 steps and due to its symmetry, 4 positive steps and 4 negative steps are required. The absolute value of the positive steps and the negative steps are equal. The symmetry of sinewave approximation 300 restricts the frequency of clock signal 209 to only integer multiples of 4 times
 20 the frequency of sinewave 300.

 Since we have assumed that the frequency of clock signal 209 must be related to the frequency of sinewave approximation 300 by an integer multiple of 4 and that the same step sizes must be used in each quadrant of the square wave, the symmetry of the
 25 sinewave approximation 300 may be exploited in order to simplify the calculation of the Fourier Transform. Furthermore, sinewave approximation 300 has odd symmetry, we need only keep the sine terms in the calculation of the Fourier Transform. If we denote the sinewave frequency as ω_0 , then the Fourier Transform of the
 30 multiplying waveform will be given by:

$$f(t) = \sum_{n=0}^{n=\infty} A_n \sin(n\omega_0 t)$$

where

$$A_n = \frac{2}{\pi} \int_0^{\pi} f(t) \sin(n\theta) d\theta$$

- 5 In the example that is shown in FIG. 3, there are four steps that are used to approximate the curvature of the sinewave. The step values are S_0 , S_1 , S_2 and S_3 . In order to simplify the Fourier Transform calculation it is convenient to define a new set of variables. These variables are:

10

$$\begin{aligned} K_0 &= S_0 \\ K_1 &= (S_1 - S_0) \\ K_2 &= (S_2 - S_1) \\ K_3 &= (S_3 - S_2) \end{aligned}$$

The A_n coefficients may now be found in terms of the K_n coefficients as:

15

$$A_n = \frac{4}{n\pi} \sin\left(\frac{n\pi}{2}\right) \left[K_0 \sin\left(\frac{4n\pi}{8}\right) + K_1 \sin\left(\frac{3n\pi}{8}\right) + K_2 \sin\left(\frac{2n\pi}{8}\right) + K_3 \sin\left(\frac{n\pi}{8}\right) \right]$$

- For the general case when N is not equal to 16 the A_n coefficients are:
- 20

$$A_n = \frac{4}{n\pi} \sin\left(\frac{n\pi}{2}\right) \left[\sum_{i=0}^{i=\frac{N}{4}-1} K_{\left(\frac{N}{4}-1-i\right)} \sin\left(\frac{2n\pi i}{N}\right) \right]$$

- Three important observations may be made from an examination of the above equation.
- 25

$$A_n = 0 \quad \text{for even } n$$

$$A_{N+n} = A_n \quad (\text{except for the factor of } \frac{1}{n})$$

$$A_{N-n} = -A_n \quad (\text{except for the factor of } \frac{1}{n})$$

Due to the repetitive nature of the A_n coefficients and the fact that $A_{N-n} = -A_n$ (except for the factor of $1/n$), we will consider only the first $N/2$ coefficients. Furthermore, since the even numbered coefficients are equal to zero, it is only necessary to consider the first $N/4$ odd coefficients. For the example given ($N=16$), the first $N/4$ odd coefficients are A_1, A_3, A_5 and A_7 . The A_1 term gives us our desired mixing product, while the other terms give undesired harmonic signals which we will attempt to remove. Since there are 4 unknowns (the 4 step sizes), 4 of the A_n coefficients may be chosen arbitrarily. The first $N/4$ odd A_n coefficients are chosen as follows:

$$A_1 = 1.0$$

$$A_3 = 0.0$$

$$A_5 = 0.0$$

$$A_7 = 0.0$$

Due to the repetitive nature of the A_n coefficients the next $N/4$ odd A_n coefficients are given by:

$$A_9 = 0.0$$

$$A_{11} = 0.0$$

$$A_{13} = 0.0$$

$$A_{15} = \frac{-A_1}{n} = \frac{-1}{15}$$

Since there are $N/4$ unknowns (the K_n coefficients) and $N/4$ knowns (the A_n coefficients) a set of $N/4$ equations may be written

which relate the K_N coefficients to the A_N coefficients. These equations may be solved using any number of techniques. For the example given ($N=16$) the results are:

$$\begin{array}{ll} K_0 = 0.1963495408 & S_0 = 0.1963495408 \\ K_1 = 0.3628066440 & S_1 = 0.5591561849 \\ K_2 = 0.2776801836 & S_2 = 0.8368363685 \\ K_3 = 0.1502794325 & S_3 = 0.9871158010 \end{array}$$

With this mixer design, the only non zero harmonics of the multiplying waveform which will appear at the mixer output, will be values of n which satisfy the following equation.

10

$$n = iN \pm 1 \quad \text{where} \quad i = 0, 1, 2, 3, \dots$$

The non zero A_N coefficients are related to A_1 in the same manner as the simple square wave.

15

$$|A_n| = \frac{|A_1|}{n}$$

In order to simplify the circuit design it is desirable to scale the step sizes so that the value of the maximum step size is equal to 1.0.

20 The only effect that this simplification will have is a slight change in the gain of the mixer. For the example given ($N=16$) the new coefficients are:

$$\begin{array}{l} S'_0 = 0.19891237 \\ S'_1 = 0.56645450 \\ S'_2 = 0.84775907 \\ S'_3 = 1.00000000 \end{array}$$

25

These coefficients are shown in FIG. 3. The table shown below gives the first 31 harmonic levels for the conventional

switching mixer and the new mixer (N=16). The harmonic levels are given in dB relative to the desired harmonic (n=1). The even order harmonics are not shown since they are zero ($-\infty$ dB) for both mixers.

5

n	Conventional Mixer	New Mixer
1	0.00	0.00
3	- 9.54	- ∞
5	- 13.98	- ∞
7	- 16.90	- ∞
9	- 19.08	- ∞
11	- 20.83	- ∞
13	- 22.28	- ∞
15	- 23.52	- 23.52
17	- 24.61	- 24.61
19	- 25.56	- ∞
21	- 26.44	- ∞
23	- 27.23	- ∞
25	- 27.96	- ∞
27	- 28.63	- ∞
29	- 29.25	- ∞
31	- 29.83	- 29.83

TABLE 1

10

FIG. 4 generally depicts the predetermined circuitry of the preferred embodiment of multiplying D/A convertor 206 in accordance with the invention. As shown in FIG. 4 a plurality of resistors designated by resistors R1-R8 are connected to an amplifier 400. Switching gates G1-G8 are utilized to switch

15

resistors R1-R8 into and out of the predetermined circuitry via a control word output by counter/controller 203. In the preferred

embodiment, the control word is a 3-bit control word. Also in the preferred embodiment, resistors $R1$ and $R8 = 15.22 \text{ K}\Omega$, $R2$ and $R7 = 28.13 \text{ K}\Omega$, $R3$ and $R6 = 36.76 \text{ K}\Omega$ and $R4$ and $R5 = 19.89 \text{ K}\Omega$ which, when programmed, yield coefficients $S_0'-S_3'$ calculated above.

Operation of predetermined circuitry 206 which comprises multiplying D/A convertor 206 is as follows. Clock signal 209 having a predetermined clock cycle rate ($16F_{10}$ in the preferred embodiment) is input into counter/controller 203. For every clock cycle, counter/controller 203 outputs a predetermined control word based on the coefficients $S_0'-S_3'$ as calculated above. For a given control word, gates $G1-G8$ switch into and out of certain resistors $R1-R8$ based on the control word. This yields a certain multiplication ratio for circuitry 206 which changes every clock cycle as the control word changes. Consequently, the result of circuitry 206 changing every clock cycle is that an input signal V_{in} is multiplied by step sizes (based on the coefficients $S_0'-S_3'$ as calculated above) which, as a function of time, approximate sinewave approximation 300. In this manner, the advantages of a switching mixer are obtained without the exhibition of odd harmonics at the output of the mixer.

What we claim is:

Claims

- 5 1. An apparatus for frequency translation comprising:
- a clock signal having a predetermined clock cycle rate;
- a controller for outputting a predetermined control signal every clock cycle; and
- 10 a multiplying digital-to-analog convertor having a multiplication ratio based on the control signal, the multiplying digital-to-analog convertor multiplying an input signal by step sizes which, as a function of time, approximate a sinewave.
- 15 2. The apparatus of claim 1 wherein the control signal further comprises a control word.
3. The apparatus of claim 2 wherein the multiplication ratio based on the control word further comprises switching a plurality
- 20 of resistors into and out of predetermined circuitry via a plurality of switches, the plurality of switches controlled by the control word.
4. The apparatus of claim 3 wherein the step sizes are non-
- 25 linear and are optimally determined based on switching a plurality of resistors having optimized values into and out of predetermined circuitry via the plurality of switches controlled by the control word.
- 30 5. The apparatus of claim 1 wherein the step sizes which approximate a sinewave as a function of time further comprise step sizes which approximate a sinewave over 16 clock cycles.

6. A method of frequency translation comprising:

providing a clock signal having a predetermined clock cycle rate;

5 outputting a predetermined control signal every clock cycle; and

multiplying an input signal by a multiplication ratio based on the control signal, the multiplication ratio related to step sizes which, as a function of time, approximate a sinewave.

10

7. The method of claim 6 wherein the control signal further comprises a control word.

8. The method of claim 7 wherein the step of multiplying an
15 input signal by the multiplication ratio based on the control word further comprises the step of switching a plurality of resistors into and out of predetermined circuitry via a plurality of switches, the plurality of switches controlled by the control word.

20 9. The method of claim 8 wherein the step sizes are non-linear and are optimally determined based on switching a plurality of resistors having optimized values into and out of predetermined circuitry via the plurality of switches controlled by the control word.

25

10. The method of claim 6 wherein the step sizes are linear step sizes.

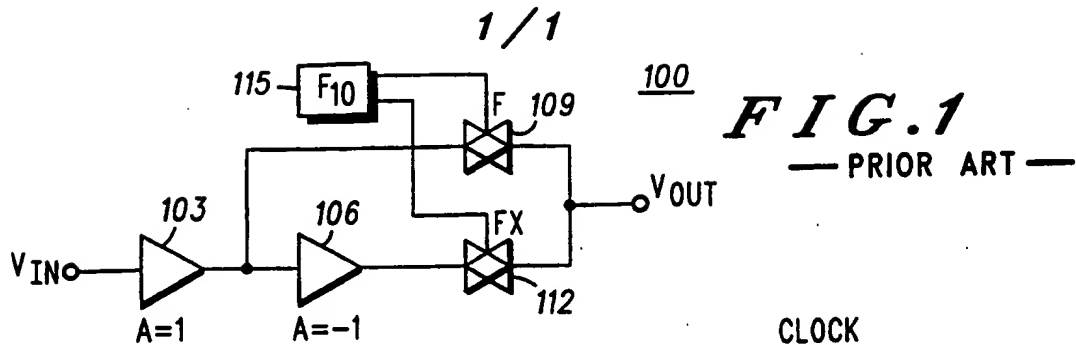


FIG. 2

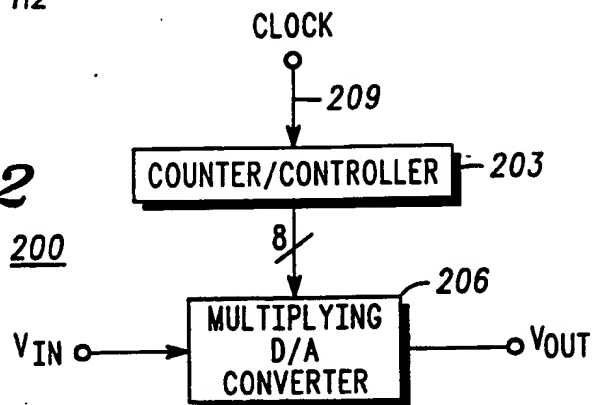


FIG. 3

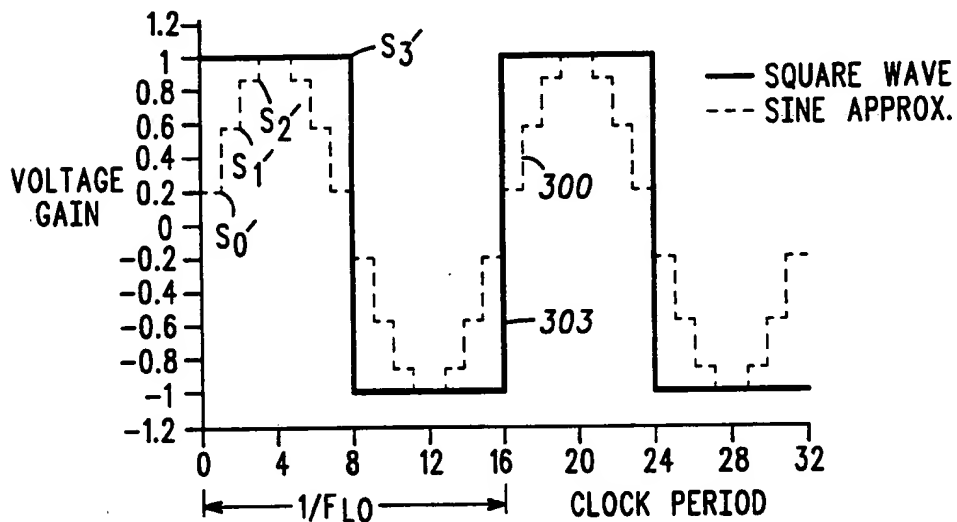
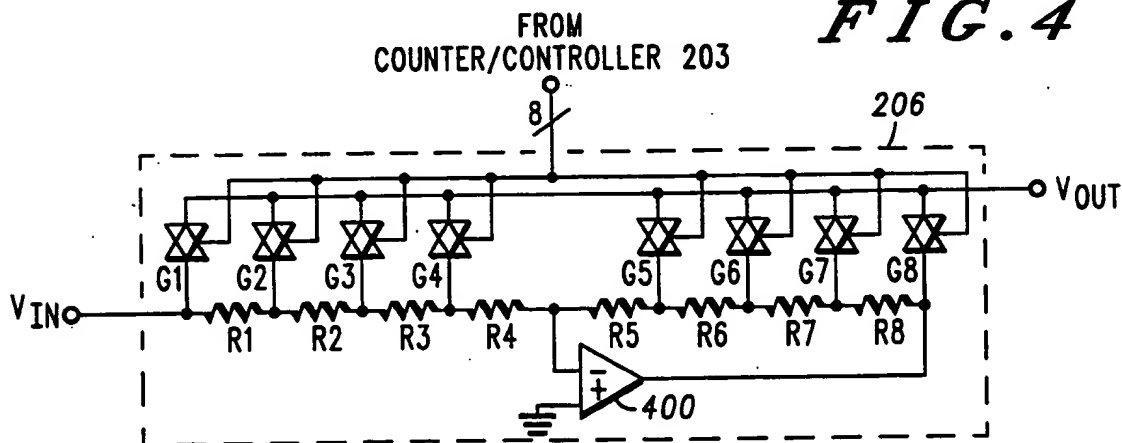


FIG. 4



INTERNATIONAL SEARCH REPORT

International application No.
PCT/US94/05419

A. CLASSIFICATION OF SUBJECT MATTER

IPC(5) :H03M 1/66

US CL : 341/144

According to International Patent Classifications (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

U.S. : 341/144, 147, 61

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

APS

search terms: multiplying dac, sine approximation, frequency

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X ----- Y	US, A, 4,727,752 (PETERS) 01 March 1988, col. 5-7.	1-4, 6-10 ----- 5

☐ Further documents are listed in the continuation of Box C. ☐ See patent family annex.

* Special categories of cited documents:	* T	later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
* A		document defining the general state of the art which is not considered to be of particular relevance
* E		earlier document published on or after the international filing date
* L		document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)
* O		document referring to an oral disclosure, use, exhibition or other means
* P		document published prior to the international filing date but later than the priority date claimed
	* X	document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
	* Y	document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art
	* G	document member of the same patent family

Date of the actual completion of the international search

05 OCTOBER 1994

Date of mailing of the international search report

19 OCT 1994

Name and mailing address of the ISA/US
Commissioner of Patents and Trademarks
Box PCT
Washington, D.C. 20231

Facsimile No. (703) 305-3230

Authorized officer

LOGAN, SHARON

Telephone No. (703) 308-1676